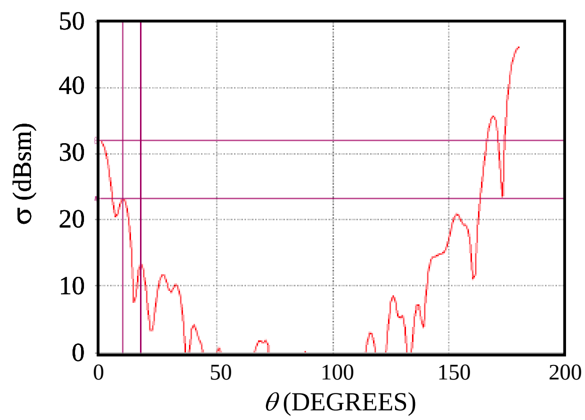
Errata to ***Radar and Laser Cross Section Engineering***, Second Edition

Location	**Reads as:**	**Should read as:**
p. 4, Eq. (1.10)	$f_c = (f_2 - f) / 2$	$f_c = (f_2 + f) / 2$
p. 6, Ex. 1.1	peak transmitter power = 200 kW $N_o = k_B T_e B$	peak transmitter power = 500 kW, $N_o = k_B T_s B$
p. 19, Ex. 1.3, Figs. 1.19 and 1.20	The plots in the figures are for an antenna efficiency of *e* = 0.85 rather than 0.5 as stated in the example. Thus the maximum range shown is 63 km, not 46 km.	
p. 19, Ex. 1.3	Last paragraph, reference to Example 1.2 should reference Example 1.1	
p. 47, Fig. 2.6	Magnetic image for PMC: $\rightarrow\rightarrow$	$\leftarrow\leftarrow$ (reverse direction)
p. 63, Fig. 2.22	$\lvert E \rvert^2 / \lvert E_o \rvert^2$	$\lvert E \rvert / \lvert E_o \rvert$
p. 68, Fig. 2.27, axes labels	$y\,(n), \quad x\,(m)$	$v\,(n), \quad u\,(m)$
p. 108, Eq. (3.55) and Eq. (3.57) two places	$j\eta / k$	$j\eta / k^2$
p. 108, Eq. (3.56) In integral limits	$(\Delta 2)$	$(\Delta / 2)$
p. 108, Eq. (3.60) in integral limits	$-L$ to L	$-L/2$ to $L/2$
p. 110, Fig. 3.8	Triangles and Pulses should be switched in the legend.	
p. 118, heading	3.6.3 Other Basic Functions	3.6.3 Other Basis Functions
p. 146, Prob. 3.13	edge (14)	edge (24)
p. 123, Ex. 3.4	… 250 MHz is due to a resonance condition for the wing.	… 270 MHz is due to a resonance condition for the fuselage.
p. 124, Fig. 3.21	Nose on RCS…	Broadside RCS…
p. 146, Pr. 3.10d	$g = k\hat{r} \bullet \vec{r}'$	$g = \hat{r} \bullet \vec{r}'$
p. 211, Fig. 4.43 The bottom figure is a repeat of the top figure. The correct bottom figure is shown here.		
p. 236, after Eq. (5.43)	$\alpha(\phi^{\pm}) = \cdots$	$a(\phi^{\pm}) = \cdots$
p. 272, Fig. 6.12	$\Omega = 2 / \ln(2a\ell)$	$\Omega = 2\ln(2\ell / a)$
p. 273, Ex. 6.5	Should be specified: $d_x = 0.5\lambda, \quad d_y = 0.45\lambda$	
p. 313, Eq. (6.88)	$\cos^2\theta$	$\cos\,\theta$
p. 324, Fig. 6.61	$N_x = 25$	$N_x = 26$
p. 327, Ref. 17	Monk	Munk

p. 361, Fig. 7.22	Labels *d* and *s* in the figure should be interchanged. With reference to text below Eq. (7.40), *d* = ring spacing.	
p. 366, Ex. 7.9	0.1 mm, $\mathrm{Re}[\mu_r] = 1$	0.1 m, $\mathrm{Re}[\mu_r] = 1.103$
p. 371, 3rd paragraph	…based the type of target…	…based on the type of target…
p. 387, Ref. 14	AP, No. 4	AP-11, No. 5
p. 393, Pr. 7.21	The PML of Problem…	For the PML of Problem…
p. 406, Eq. (8.5)	$\sqrt{1+\frac{2d\cos\phi}{R_o} \approx R_o + d\cos\phi}$	$\sqrt{1+\frac{2d\cos\phi}{R_o}} \approx R_o + d\cos\phi$
p. 415, Eq. (9.5)	$\mathrm{d}\Phi$	$\mathrm{d}^2\Phi$
p. 431, Eq. (9.54)	$\mathcal{R}_d$	$\mathcal{R}_d^2$
p. 433, Fig. 9.26	$\tau_1\Gamma_2 E_o$	$\tau_1^2\Gamma_2 E_o$
p. 434, top line	It should be noted that *T* and *R* are **power** coefficients.	
p. 434, Eq. (9.64)	$\frac{\lvert E_T\rvert}{\lvert E_0\rvert} = \frac{\tau_1^2\tau_2^2}{1+\Gamma_1\Gamma_2 - 2\Gamma_1\Gamma_2\cos\delta}$	$\frac{\lvert E_T\rvert^2}{\lvert E_0\rvert^2} = \frac{\tau_1^2\tau_2^2}{1+\Gamma_1^2\Gamma_2^2 - 2\Gamma_1\Gamma_2\cos\delta}$
p. 434, Eq. (9.65)	$R = \frac{\Gamma_1^2+\Gamma_2^2 - 2\Gamma_1\Gamma_2\cos\delta}{1+\Gamma_1\Gamma_2 - 2\Gamma_1\Gamma_2\cos\delta}$	$R = \frac{\Gamma_1^2+\Gamma_2^2 - 2\Gamma_1\Gamma_2\cos\delta}{1+\Gamma_1^2\Gamma_2^2 - 2\Gamma_1\Gamma_2\cos\delta}$
p. 435 Eq. (9.67)	$R = \frac{(\Gamma_1+\Gamma_2)^2}{(1+\Gamma_1\Gamma_2)}$	$R = \frac{(\Gamma_1+\Gamma_2)^2}{(1+\Gamma_1\Gamma_2)^2}$